

**ANNEX F TO CRITIQUE OF ALL NASA MARS WEATHER DATA,  
WITH EMPHASIS ON PRESSURE:**

Percent Difference Flow Chart for Viking-1 Sols 1 to 113, and 134 to 350  
(Based on data from [http://www-k12.atmos.washington.edu/k12/resources/mars\\_data-information/data.html](http://www-k12.atmos.washington.edu/k12/resources/mars_data-information/data.html))

Annex F sums up the percent differences between Viking-1 measured pressures, for its Sols 1 to 113 and 134 to 350, and its predicted pressures as found in Appendices 1 and 2 to Annex D. Annex F only shows whether each pressure predicted had less than a 2% percent difference from what was measured. Where this was the case, the cell appears in red and the temperature (Kelvin) is indicated with white font in the red cell. Where the percent difference was greater than 2%, the cell is left uncolored. From Annex F it is readily apparent that when the heater had to come, the pressure at the transducer was forced up and into line with the pressure predicted for a gas being heated in a confined (dust clot,

sealed space). For example, there was less than a 2% difference at the 0.3 time-bins every day between VL-1 sols 211 and 287. This corresponds to about 7:23 AM Local True Solar Time, a good time to warm up equipment for morning operations. There was also a consistent series of good agreements with the predictions for afternoon operations and late night operations when it was necessary to prevent damage to the lander equipment. The time of the best agreement shifted as the year progressed from summer to winter. Figure 1 shows the overall success rate for predicting pressures in each cell (336 sols \* 25 time-bins per cell = 8,400 predictions).

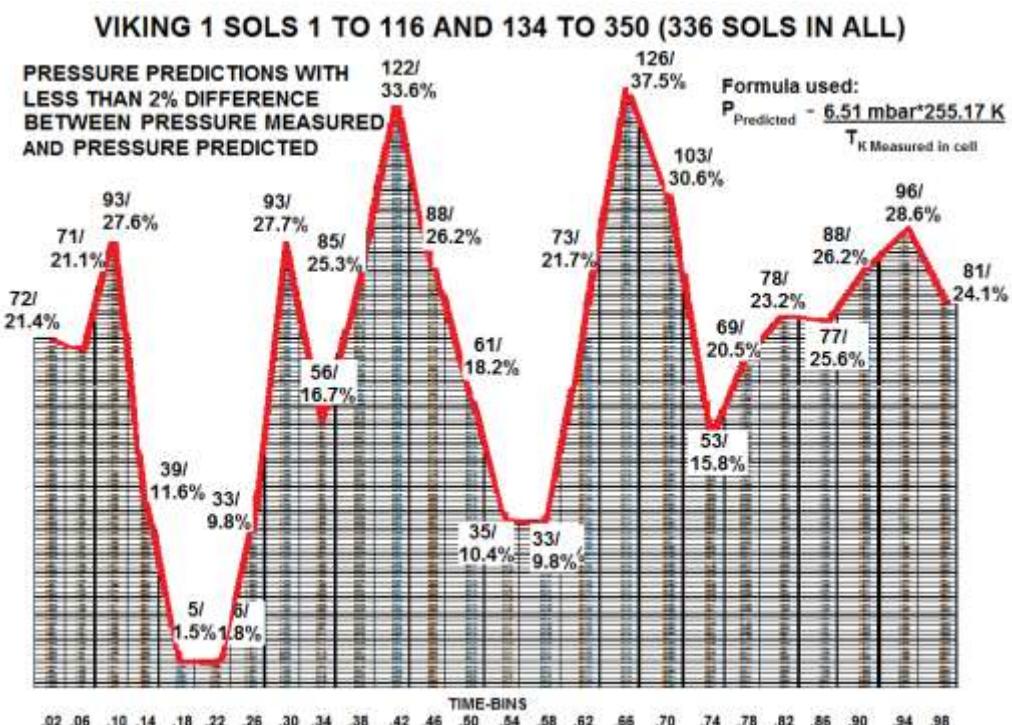
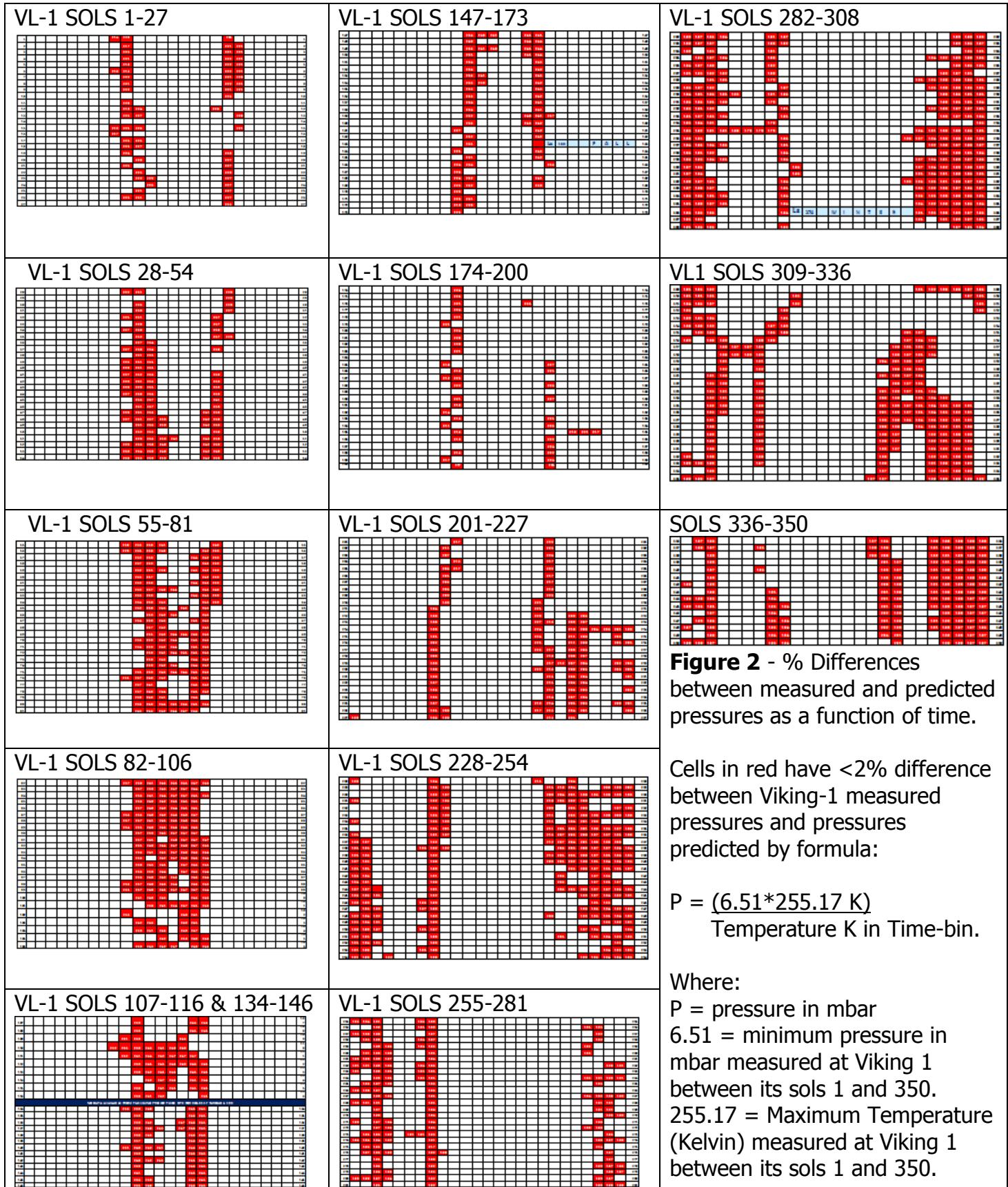


Figure 1 – Prediction success totals per time-bin and corresponding % of successful predictions.



It can be seen from Figure 2 that there was a first degree of moderate success in accurately predicting pressures in the mornings around the .38 and .42 time bins from the Viking-1 landing until its Sol 116 when data suddenly stopped until sol 134. There was also a good degree of success in making predictions in the afternoons for the 0.7 to the 0.78 time-bins, gradually shifting to the 0.62 to 0.66 time-bins, then merging with the morning success just before data stopped. So the predictions became accurate for the time-bins from about 0.42 to 0.66. This was all in the summer.

After the data break, predictions were generally better than 2% off for the 0.42, 0.62 and 0.66 time-bins for the rest of the summer. As fall ensued, the morning accuracy shifted earlier into the 0.38, then 0.34 and finally the 0.3 time-bin that first caught my attention.

In line with the expectation that the heater would have to come on and increase pressures the most as it got colder outside, the predictions grew better over more night time-bins as the fall came to an end and winter ensued. As the study came to an end on sol 350, there were often very accurate predictions for the hours centering around midnight and for several hours on either side of that time.

Professor James Tillman has been helpful a number of times in this study, which could never have occurred without his Viking Project's efforts in posting the data that my father and I to reformat and manipulate. However, the one question that Professor Tillman has not answered pertains to the thermostat or timer employed for the RTGs. Just

what caused the heaters to come on when they did? At best, without a definitive answer from him, his team, or other competent authority, the only solution is to let the data speak for itself. That data seems to indicate that if there was a timer, its settings were gradually shifted as the summer drifted into fall, and finally winter arrived.

The size of the errors, at least initially, was also particularly telling. For example, as one flips through Appendices 1 and 2 to Annex D, it is apparent that often in early hours of the sols, rows are shaded in yellow or blue. This means that there was no recorded pressure change for at least four hours, often at times when it was most cold. The blue shading means that the temperature was colder than -75° C (198.15 K), and often it was colder than -85° C (188.15 K) then. This would be a time that my formula would predict the highest temperatures, but something was not working right when it came to recording and transmitting the pressures felt at the transducer.

Did the formula work for warm and cold temperatures seen across the 336 sols studied? Yes. To see this it is necessary to look at the temperatures shown in white fonts in the red cells of Appendix 1 to this Annex and in Appendix 2 to this Annex which is a histogram of the temperatures that produced under a 2% difference between measured and predicted pressures.

VL1 SOL	0.02	0.06	0.1	0.14	0.18	0.22	0.26	0.3	0.34	0.38	0.42	0.46	0.5	0.54	0.58	0.62	0.66	0.7	0.74	0.78	0.82	0.86	0.9	0.94	0.98	VL1 SOL
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1									214	220									224							1		
2										217										221	221						2	
3										223										221	221						3	
4										221										222	221						4	
5										218										222	221						5	
6									218	216										222	221						6	
7										222										221	220						7	
8										221										222	221						8	
9										222										221	221						9	
10																				226							10	
11										220																	11	
12										219	224									228							12	
13										223	227										220							13
14																												14
15										219	225	226									221							15
16										217																	16	
17											223	225															17	
18											223	227															18	
19											224										230							19
20												228									227							20
21											223										227							21
22											223										228							22
23											222	229									227							23
24												226									227							24
25											221										227							25
26											223	231									227							26
27																				233							27	

VL1 SOL	0.02	0.06	0.1	0.14	0.18	0.22	0.26	0.3	0.34	0.38	0.42	0.46	0.5	0.54	0.58	0.62	0.66	0.7	0.74	0.78	0.82	0.86	0.9	0.94	0.98	VL1 SOL
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VL1	0.02	0.06	0.1	0.14	0.18	0.22	0.26	0.3	0.34	0.38	0.42	0.46	0.5	0.54	0.58	0.62	0.66	0.7	0.74	0.78	0.82	0.86	0.9	0.94	0.98	VL1 SOL
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28										222	231								228							28
29																			229							29
30											226								228							30
31											230								227							31
32										225	231							237							32	
33											228							237							33	
34										227	230						238							34		
35											232						237	229							35	
36											227	234													36	
37										227	230	234						238							37	
38											231	235													38	
39										226	231	235													39	
40										228	231	235													40	
41										227	232	236						239							41	
42										229	231	236						239							42	
43										228	229	235						239							43	
44										227	230	236						239							44	
45											233	237						241							45	
46										231	237						239								46	
47										228	231	236					241	239							47	
48										227	231	237	239				242	238							48	
49											231	236	239				242	239							49	
50											232	236						238							50	
51											229	236	239	241				243	239						51	
52										229	233	238	240				242	239							52	
53										230	234	238	240				242	240							53	
54										230	233	239	239				242	239							54	

VL1	0.02	0.06	0.1	0.14	0.18	0.22	0.26	0.3	0.34	0.38	0.42	0.46	0.5	0.54	0.58	0.62	0.66	0.7	0.74	0.78	0.82	0.86	0.9	0.94	0.98	VL1 SOL
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55									230	233	238	241						240							55	
56									229	235	238	240						242	239						56	
57									232	238								244	242	239					57	
58									237	239								243	239						58	
59									232	235	238							243	242	239					59	
60									233	237								242	239						60	
61									232	238								244	243	239					61	
62									232	237	240	244						243	240						62	
63									233	239								244	243	239					63	
64									234	238	243							243	239						64	
65									232	238	243							243							65	
66										239	242	243						243							66	
67									234	239	243							245	243						67	
68										237	242							243							68	
69										235	242	244	244					246	243						69	
70										236	239	242	244					245	243						70	
71										234	239	242	244					245	243						71	
72											238	241	244	245					245	243						72
73											238	243							244	242						73
74											239	242	244						244	242						74
75											235	239	243	244	244				245	243						75
76											235	237	240	242					245	243						76
77												237	241						246	242						77
78												237	240	244					245	242						78
79												238	240	241					244							79
80												236	240	244	245	244			245	244						80
81												243	246	242	244	247			244							81

VL1 SOL	0.02	0.06	0.1	0.14	0.18	0.22	0.26	0.3	0.34	0.38	0.42	0.46	0.5	0.54	0.58	0.62	0.66	0.7	0.74	0.78	0.82	0.86	0.9	0.94	0.98	VL1 SOL
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VL1 SOL	0.02	0.06	0.1	0.14	0.18	0.22	0.26	0.3	0.34	0.38	0.42	0.46	0.5	0.54	0.58	0.62	0.66	0.7	0.74	0.78	0.82	0.86	0.9	0.94	0.98	VL1 SOL
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82									237	238	241	246	245	245	247	246										82		
83									237	239	243	247	247	244												83		
84									236	241	244	247	247	245	245	243										84		
85									236	240	242	245	245	245	245											85		
86									237	240	242	244	245	245	245											86		
87									236	236	240	242	246	249	247											87		
88									237	237	241	245	245	248	246											88		
89									234	235	240	243	246	246	246											89		
90										237	239	243	247	247	247	247										90		
91										237	245		248	247	247	247											91	
92										235	240	244	247	248	247	245										92		
93										236	241	243	247	248	246	244										93		
94										236		242	247	248	246	244											94	
95										238	243	245		247	246	245											95	
96										236	239	244		247	246	244											96	
97										236	240	242	246		246	244											97	
98										236	237	240	243	244		246	243										98	
99										235	237	240	245	247	247	247	244									99		
100											241	240	243			246	243										100	
101											238	241	244	247	245	243											101	
102										236					248	241												102
103											242	246			249	245											103	
104											239	241	246		249	247											104	
105												242			250	248	246										105	
106											239	243	242	247		248	246										106	

VL1 SOL	0.02	0.06	0.1	0.14	0.18	0.22	0.26	0.3	0.34	0.38	0.42	0.46	0.5	0.54	0.58	0.62	0.66	0.7	0.74	0.78	0.82	0.86	0.9	0.94	0.98	VL1 SOL
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VL1	0.02	0.06	0.1	0.14	0.18	0.22	0.26	0.3	0.34	0.38	0.42	0.46	0.5	0.54	0.58	0.62	0.66	0.7	0.74	0.78	0.82	0.86	0.9	0.94	0.98	VL1 SOL
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107										239						246	246									10 7
108										239						245	245									10 8
109									231	239					246											10 9
110								232	233	238	243	241	248	248												11 0
111								232	241	244	242	247	247	247												11 1
112									239	245	245	246	249	246	245											11 2
113									238	242	245	246			245	245										11 3
114										242	247	246			245	244										11 4
115									238		241	245			245	245										11 5
116									238	241	242					245										11 6

NO DATA AVAILABLE FROM THE VIKING PROJECT WEB SITE FOR SOLS 117 THROUGH 133

134								233	239	240					245	245										134
135									239						246	245										135
136									239	242				247	246	245										136
137									239	240	243			247	246	245										137
138									238	243					246	246										138
139									237						246	245										139
140								231	240	242	241				246	245									140	
141									239						245	245										141
142									240	242	243				245	245										142
143									239						246	245										143
144									241						245	245										144
145									236	239					246	245										145
146									235	240					246	245										146

VL1	0.02	0.06	0.1	0.14	0.18	0.22	0.26	0.3	0.34	0.38	0.42	0.46	0.5	0.54	0.58	0.62	0.66	0.7	0.74	0.78	0.82	0.86	0.9	0.94	0.98	VL1 SOL
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VL1	0.02	0.06	0.1	0.14	0.18	0.22	0.26	0.3	0.34	0.38	0.42	0.46	0.5	0.54	0.58	0.62	0.66	0.7	0.74	0.78	0.82	0.86	0.9	0.94	0.98	VL1 SOL
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147										234	240	241			245	245										147				
148										240					244	244											148			
149										236	241	240			245	244											149			
150										235					245	244											150			
151										234					243													151		
152										234					242													152		
153										236	241				243													153		
154										233	239				242													154		
155										233					243														155	
156										233					242														156	
157										234					241														157	
158										234					241														158	
159										232					240	241	237											159		
160										236					243	242												160		
161										227						242													161	
162										232						242													162	
163										235							Ls	180						F	A	L	L	163		
164										225						243													164	
165										231						242													165	
166										224	234						236												166	
167										226																				167
168										224	232						241												168	
169										223	232						239												169	
170										229																				170
171										223	231																		171	
172										219	228																		172	
173										223																				173

VL1	0.02	0.06	0.1	0.14	0.18	0.22	0.26	0.3	0.34	0.38	0.42	0.46	0.5	0.54	0.58	0.62	0.66	0.7	0.74	0.78	0.82	0.86	0.9	0.94	0.98	VL1 SOL
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VL1 SOL	0.02	0.06	0.1	0.14	0.18	0.22	0.26	0.3	0.34	0.38	0.42	0.46	0.5	0.54	0.58	0.62	0.66	0.7	0.74	0.78	0.82	0.86	0.9	0.94	0.98	VL1 SOL
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174										224																174	
175										226																175	
176										221																176	
177										224																177	
178										221																178	
179										221																179	
180										224																180	
181										220																181	
182										220																182	
183										221																183	
184																											184
185										218																185	
186										218																186	
187										212	223															187	
188										222																188	
189																											189
190										221																190	
191										218																191	
192										214																192	
193										216																193	
194										211																194	
195										216																195	
196										219																196	
197																											197
198										216																198	
199										217																199	
200										217																200	

VL1 SOL	0.02	0.06	0.1	0.14	0.18	0.22	0.26	0.3	0.34	0.38	0.42	0.46	0.5	0.54	0.58	0.62	0.66	0.7	0.74	0.78	0.82	0.86	0.9	0.94	0.98	VL1 SOL
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VL1 SOL	0.02	0.06	0.1	0.14	0.18	0.22	0.26	0.3	0.34	0.38	0.42	0.46	0.5	0.54	0.58	0.62	0.66	0.7	0.74	0.78	0.82	0.86	0.9	0.94	0.98	VL1 SOL
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201									217									222								201		
202									211									223								202		
203									207									224								203		
204									213									217								204		
205									206	217								222								205		
206									205									217								206		
207									206									217								207		
208									206									218								208		
209									209									223								209		
210									199									221								210		
211									194									225								211		
212									198									229			209	206				212		
213									198									227	219		209	207				213		
214									199									224			210	208	204	203	201	199	214	
215									195									224			211	208			203		215	
216									202									225			211	208			205	205	216	
217									200									223	217		209	206					217	
218									200									218			208	207					218	
219									199									217	212	207	204			202	203		219	
220									198									222	216		208	206			203	205		220
221									198									215			206	204			201		221	
222									197									215			206	204					222	
223									196									212			206	203			202		223	
224									196									214			207	204					224	
225									197									219	214		205	203			200	201		225
226									195	200							217	213		204	201			200		226		
227	199								196	199							213			205						227		

VL1 SOL	0.02	0.06	0.1	0.14	0.18	0.22	0.26	0.3	0.34	0.38	0.42	0.46	0.5	0.54	0.58	0.62	0.66	0.7	0.74	0.78	0.82	0.86	0.9	0.94	0.98	VL1 SOL
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VL1	0.02	0.06	0.1	0.14	0.18	0.22	0.26	0.3	0.34	0.38	0.42	0.46	0.5	0.54	0.58	0.62	0.66	0.7	0.74	0.78	0.82	0.86	0.9	0.94	0.98	VL1 SOL
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228	198							194									215			204						228	
229								196	199								215	210	204			200	199	202		229	
230								192	197								209	204	201	198	196	198	198	199	198	230	
231	196							192	196								210	206	202	200						231	
232								193	199								209		203	200			197	199		232	
233								193	199								211		203	200	198	198	200	198		233	
234	197							193	199								211		304	201	200						234
235								195	201								211	205	203	201	198	196	197	198		235	
236	195							191	197								213	207	203	200	197	197	195	198		236	
237	198	197						192									212	207	204	201	198	198	200			237	
238	195	193						193	192	192								206	203	200	197	197	196	194		238	
239	195	196						192										213	205	203	200	197	195	196	196		239
240	197	193						190										209	205	202	198	195	194	194	193		240
241	195	195						189											203	200	197	195	195	195	197		241
242	196	194						191										206				197	196				242
243	194	191						190										206				197	195	197			243
244	197	197						191										206	203	200	197	197	196	195		244	
245	196	196	195					192												199	197	194	192	191		245	
246	190	189						186	189											195	193					246	
247		193	189					187	189											198	196	194	192	190		247	
248	192	194	192					189										208			199	196	195	194	192		248
249	193	194	191					189														193	192	191			249
250	190	189	187					185	187											197	194				194		250
251	192	193						188										205			196	194	193	193		251	
252	195	194	193					189														191					252
253	191	188						185	188												194	193	193			253	
254	191	189		192				190												199	196	194	194	193		254	

VL1	0.02	0.06	0.1	0.14	0.18	0.22	0.26	0.3	0.34	0.38	0.42	0.46	0.5	0.54	0.58	0.62	0.66	0.7	0.74	0.78	0.82	0.86	0.9	0.94	0.98	VL1 SOL
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VL1 SOL	0.02	0.06	0.1	0.14	0.18	0.22	0.26	0.3	0.34	0.38	0.42	0.46	0.5	0.54	0.58	0.62	0.66	0.7	0.74	0.78	0.82	0.86	0.9	0.94	0.98	VL1 SOL
------------	------	------	-----	------	------	------	------	-----	------	------	------	------	-----	------	------	------	------	-----	------	------	------	------	-----	------	------	------------

255	193	194	191				186	189																		255		
256			190				185	188															195	193		256		
257	193	190	188					187																192			257	
258		193	189				184	187															192			258		
259			188	186			184	186														192			259			
260		191	189	188				185													193				260			
261	189	189	189	187				184																			261	
262	191	191	188	186			184	186															190	191		262		
263	191		188	185			183	185																			263	
264			189	185			183	185													193	191	189	191	264			
265		186	187	190				186													193					265		
266	190	190	187					186																				266
267			189	186				185													194	192	190	189		267		
268	190	191	191					185													191	191				268		
269			187					184													191	191				269		
270			189					184													189	189				270		
271	189		187	184				184													190					271		
272			187	186				183													190	188				272		
273		185	183	182			181	181	183													186					273	
274	186	184	184	182				181													188	187	188			274		
275		183	183					217													224						275	
276		187	183	182				182	188												187					276		
277			185					188													187						277	
278			186					182													189	187	186			278		
279			186	186				183													188	187				279		
280	189	189	187	184				182													189	187				280		
281			185					182													189	188	188			281		

VL1 SOL	0.02	0.06	0.1	0.14	0.18	0.22	0.26	0.3	0.34	0.38	0.42	0.46	0.5	0.54	0.58	0.62	0.66	0.7	0.74	0.78	0.82	0.86	0.9	0.94	0.98	VL1 SOL
------------	------	------	-----	------	------	------	------	-----	------	------	------	------	-----	------	------	------	------	-----	------	------	------	------	-----	------	------	------------

VL1 SOL	0.02	0.06	0.1	0.14	0.18	0.22	0.26	0.3	0.34	0.38	0.42	0.46	0.5	0.54	0.58	0.62	0.66	0.7	0.74	0.78	0.82	0.86	0.9	0.94	0.98	VL1 SOL
------------	------	------	-----	------	------	------	------	-----	------	------	------	------	-----	------	------	------	------	-----	------	------	------	------	-----	------	------	------------

282	189	187	186	184					181	187														189	188	189	282					
283	188	187	187						180	182														189	186	187	283					
284	188		183						181																186	185	284					
285		186	187	184					180															194	192	189	188	186	285			
286	184	187	188						182																188	186	185	286				
287	185	183	182	182					180															189	187	185		287				
288			185	185					179															195	193	190	188	186	185	288		
289	186	187	182							187															193	190	188	186	185	289		
290	184	185	186	185	183				181	186															188	186	185	185	290			
291	186	186	185	180					179																188	186	185	184	291			
292	183	185	182							185															192	189	187	187	185	292		
293	185	187	183	184						185															190	187	185	184	293			
294	183	184	181						178																			183	294			
295	183	182	181	181	180	179	178	179																194	191	190	188	186	185	295		
296	188	183								186															198	197	194	190	188	188	296	
297	184	186	184	186						185															192	190	187	188	187	297		
298	186	185	182							184																190	188	185	184	298		
299	186	183	184	185						184															197	194	191	189	187	186	299	
300	187	186									186														197	194	192	189	188	189	300	
301	187	184									183														195	194	191	188	186	185	301	
302	188	187	185							184															199	196	193	191	188	187	186	302
303	187	188	187							185															196	192	190	187	186	187	303	
304	186	186	185	184						184															196	193	190	188	186	185	304	
305	185	188	187	185						184															194	192	190	188	186	184	305	
306	186	186	186							184	Ls	270	W	I	N	T	E	R						195	193	190	189	187	186	306		
307	185	183																							195		191	189	187	185	307	

VL1 SOL	0.02	0.06	0.1	0.14	0.18	0.22	0.26	0.3	0.34	0.38	0.42	0.46	0.5	0.54	0.58	0.62	0.66	0.7	0.74	0.78	0.82	0.86	0.9	0.94	0.98	VL1 SOL
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VL1 SOL	0.02	0.06	0.1	0.14	0.18	0.22	0.26	0.3	0.34	0.38	0.42	0.46	0.5	0.54	0.58	0.62	0.66	0.7	0.74	0.78	0.82	0.86	0.9	0.94	0.98	VI1 SOL
------------	------	------	-----	------	------	------	------	-----	------	------	------	------	-----	------	------	------	------	-----	------	------	------	------	-----	------	------	------------

308	185	186	186						183														187	185	184	308			
309	185	183	182																				195	192	190	188	187	186	309
310	185	185	185							193															187	185	310		
311	184	186	187							192																185	311		
312	186								188																	188	312		
313	189	185	184						185																		313		
314	190	188	192						187	189																	314		
315		189	189						186	188												201	197					315	
316	189		190	189					188	188												197	194	193				316	
317				188	187	187	188														198	195	193	193			317		
318				190	189	189	189														199	197	195	194			318		
319				191			191														204	201	199	197				319	
320				192			192														200	198	196					320	
321			191	190																	201	199	197	194				321	
322			193	190			190														200	197	195					322	
323			193	191			190														201	199	197	195	194			323	
324			192	191			189														200	198		195	194	192		324	
325			192	190			189														201	199	197	195	194	193	192	191	325
326			193	191			189														201	199	197	195	194	193	192	191	326
327			191				189														199	198	196	194	193	192	191	191	327
328			190				188														200	198		194	193	192	191	190	328
329			189				187														198	197			192	191	190	190	329
330			188				188														198	197			192	191	190	190	330
331			190				188														199	197			193	192	191	190	331
332	189		190				188														198				192	191	190	190	332
333	189	190	189				187														198				191	190	189	189	333
334			188																		197				191	189	188	188	334

VL1 SOL	0.02	0.06	0.1	0.14	0.18	0.22	0.26	0.3	0.34	0.38	0.42	0.46	0.5	0.54	0.58	0.62	0.66	0.7	0.74	0.78	0.82	0.86	0.9	0.94	0.98	VI1 SOL
------------	------	------	-----	------	------	------	------	-----	------	------	------	------	-----	------	------	------	------	-----	------	------	------	------	-----	------	------	------------

VL1 SOL	0.02	0.06	0.1	0.14	0.18	0.22	0.26	0.3	0.34	0.38	0.42	0.46	0.5	0.54	0.58	0.62	0.66	0.7	0.74	0.78	0.82	0.86	0.9	0.94	0.98	VL1 SOL
------------	------	------	-----	------	------	------	------	-----	------	------	------	------	-----	------	------	------	------	-----	------	------	------	------	-----	------	------	------------

335	188	188	187													197	197				190	189	188	188	188	335	
336		187	186													197	196				190	188	188	188	188	336	
337		188	187				185									199	198				191	190	189	189	189	337	
338			189													200	200				192	191	189	189	189	338	
339			189													201	197				192	191	189	189	188	339	
340			187				186									199	197				191	190	189	188	188	340	
341			189													199	198				192	190	189	188	188	341	
342	188		189													200	198				191	189	189	188	188	342	
343			188				185									201	198				191	190	188	188	188	343	
344	188	188	186				184									201	198				191	189	188	187	187	344	
345	189	186	185				183	184								201	198				191	189	188	187	187	345	
346			187				184									202	199					189	188	187	187	187	346
347		189	186				183	184								201	198				191	189	188	187	187	347	
348	187		188				183	184								202	199				191	189	187	187	186	348	
349			188				184	184								204	201					190	188	187	187	187	349
350	188	190	187				183	184								201						190	188	187	187	187	350

VL1 SOL	0.02	0.06	0.1	0.14	0.18	0.22	0.26	0.3	0.34	0.38	0.42	0.46	0.5	0.54	0.58	0.62	0.66	0.7	0.74	0.78	0.82	0.86	0.9	0.94	0.98	VL1 SOL
------------	------	------	-----	------	------	------	------	-----	------	------	------	------	-----	------	------	------	------	-----	------	------	------	------	-----	------	------	------------

0.02 time	0.06 time	0.1 time	0.14 time	0.18 time	0.22 time	0.26 time	0.3 time	0.34 time	0.38 time	0.42 time	0.46 time	0.5 time	0.54 time	0.58 time	0.62 time	0.66 time	0.7 time	0.74 time	0.78 time	0.82 time	0.86 time	0.9 time	0.94 time	0.98 time
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### HISTOGRAM FOR TIME-BINS WITH TEMPERATURES SHOWING WHERE THERE WAS <2% DIFFERENCE BETWEEN PRESSURES PREDICTED AND MEASURED

199	197	195	192	246	246	193	194	214	220	224	229	239	241	243	244	241	228	224	221	221	217	203	201	199
198	193	189	186	183	181	186	198	218	217	227	226	239	244	244	243	242	237	221	221	206	204	200	203	205
196	196	192	188	180	179	187	198	219	223	226	234	239	243	245	244	242	237	221	221	207	196	198	205	203
197	193	191	187	187	187	185	199	217	221	225	234	240	244	244	244	243	238	222	221	208	198	198	202	205
195	195	187	186	189	189	185	195	232	218	227	235	240	244	244	245	242	237	222	221	208	200	196	203	201
198	194	193	185			186	202	221	216	228	235	239	244	247	246	242	238	222	220	208	198	197	200	202
195	191	191	185			185	200	218	222	223	235	241	244	245	245	242	239	221	221	206	197	198	199	201
195	197	190	190			184	200	212	221	222	236	240	244	247	245	242	239	222	221	207	198	197	199	200
197	196	188	186			184	199	214	222	221	236	238	244	247	245	242	239	221	220	204	197	195	197	202
195	189	189	184			184	198	211	220	231	235	240	245	245	244	243	239	226	221	206	197	194	200	198
196	193	188	186			183	198	217	219	231	236	243	244	245	244	242	241	230	218	204	195	195	197	199
194	194	189	182			183	197	211	223	226	237	243	245	249	245	242	239	227	209	204	197	196	195	198
197	194	189	182			181	196	207	225	230	237	242	247	248	245	243	239	227	209	203	197	195	200	198
196	189	188	182			178	196	206	223	231	236	243	247	246	243	238	228	210	204	197	197	196	198	
190	193	188	186			188	197	205	223	228	237	242	245	247	245	243	239	227	211	203	197	194	196	194
192	194	189	184			188	195	206	224	230	236	242	244	247	244	243	238	227	211	201	197	193	194	196
193	188	187	184			189	196	206	223	232	236	242	246	248	245	243	239	227	209	198	195	194	195	193
190	189	187	184			191	194	209	223	227	236	242	245	248	244	239	227	208	200	196	195	197	197	
192	194	189	182			192	196	199	222	230	238	241	246	248	247	243	240	233	207	200	196	193	196	195
195	190	191	185			190	192	200	225	231	238	243	247	247	244	243	239	228	208	200	194	194	192	191
191	193	187	185			190	192	199	227	231	239	242	248	247	245	243	240	229	206	201	196	194	192	190
191	191	189	180			189	193	199	227	231	238	243	247	247	245	243	239	228	206	201	196	194	194	192
193	189	187	184			189	193	197	226	232	238	242	247	247	245	243	239	227	206	200	195	193	192	191
193	191	187	181			189	193	196	228	231	238	244	247	248	247	243	239	229	207	201	192	192	193	194
189	186	183	186			189	195	199	227	229	239	241	246	249	246	242	239	180	205	200	193	192	191	193
191	190	184	185			188	191	199	229	230	235	244	244	249	246	242	239	212	204	200	193	191	193	193
191	191	183	184			187	192	199	228	233	237	242	247	250	247	243	239	210	205	198	194	193	194	193
190	185	183	185			188	192	201	227	231	238	246	244	246	247	243	240	204	204	200	190	192	190	191
190	184	185	189			188	192	197	228	231	237	243	247	248	247	242	239	206	204	200	192	191	189	191
189	183	186	188			188	190	192	227	231	239	244	248	247	246	242	239	205	205	201	199	189	191	189
186	187	186	190			187	189	188	229	231	238	242	247	249	246	244	237	207	202	198	190	191	189	189
189	189	187	191			185	191	187	230	232	238	242	246	246	247	246	236	207	203	199	190	188	191	188
189	187	185	192			186	190	182	230	229	239	242	246	246	247	246	237	206	203	197	188	188	186	186
188	187	186	190			191	187	230	233	239	245	246	246	247	247	246	225	205	304	199	188	189	186	187
188	186	187	190			192	186	229	234	237	243	245	246	245	245	226	205	203	194	189	189	187	188	
184	187	183	191			189	185	235	233	235	243	247	247	244	244	227	206	203	193	190	189	224	189	
185	183	187	191			189	185	237	233	239	244	246	246	245	244	246	225	206	204	193	190	189	187	187
186	187	188	190			189	186	236	235	239	243	245	245	245	245	245	226	206	203	192	190	189	187	185
186	187	185	191			189	185	237	232	238	242	244	241	241	244	241	222	205	203	191	190	189	187	186
184	186	182	191			187	184	201	227	231	237	243	247	247	244	242	239	212	204	200	192	190	189	187
186	187	188	190			188	186	190	227	231	234	238	245	245	245	245	245	226	206	203	192	190	189	187
184	187	183	191			189	184	235	233	235	243	247	247	244	244	244	244	227	206	203	191	190	189	187
183	187	186	186			188	185	236	232	240	243	248	248	245	243	242	224	197	195	194	191	188	186	185
183	182	182	190			190	184	231	232	241	245	245	245	243	242	242	222	195	194	194	191	186	184	
188	183	183				189	184	233	233	240	243	247	247	246	245	243	223	197	197	193	190	186</		

0.02 time	0.06 time	0.1 time	0.14 time	0.18 time	0.22 time	0.26 time	0.3 time	0.34 time	0.38 time	0.42 time	0.46 time	0.5 time	0.54 time	0.58 time	0.62 time	0.66 time	0.7 time	0.74 time	0.78 time	0.82 time	0.86 time	0.9 time	0.94 time	0.98 time		
<b>HISTOGRAM FOR TIME-BINS WITH TEMPERATURES SHOWING WHERE THERE WAS &lt;2% DIFFERENCE BETWEEN PRESSURES PREDICTED AND MEASURED</b>																										
189	190	191				181	224	237	240			244	245	213		195	191	190	192	186	185					
189	188	193				217	220	235	240			245	245	215		195	191	191	191	186	188					
189	187	193				182	220	237	240			245	245	209		195	190	191	191	187	188					
188	188	192				188	221	237	238			240	244	210		195	190	190	190	187	188					
188	188	192				182	218	235	246			243	244	209		194	191	190	190	185	189					
188	186	193				183	223	236	241			235	244	211		194	192	189	191	187	189					
189	189	191				182	222	236	243			197	243	211		192	190	190	190	187	188					
187	190	190				182	221	238	243			197	242	211		191	189	189	191	188						
188						181	218	236	244			199	243	213		192	189	188	191	188						
						180	216	236	245			200	242	212		191	189	188	191	188						
						181	216	237	242			243	213			191	189	188	190	188						
						180	219	237	242			242	209			191	189	189	190	187						
						182	224	241	241			241	208			191	190	189	190	187						
						180	216	242	240			241	198			191	190	189	190	187						
						179	217	239	242			241	199			191		189	190	187						
						181	217	239	240			242	201					189	189	186						
						179	213	239	243			242	200					189	188	187						
						178	217	239	242			242	199					188	188	187						
						179	186	238	242			243	200					188	188							
						187	183	241	239			242	199					188	189							
						186	193	239	240			241	198					188	189							
						188	192	238	240			239	199					188	189							
						185	238	241				221	199					187	188							
						186	184	238	241			225	198					188	188							
						183	239	239				229	198					188	188							
						184	239					227	197					188								
						183	239					224	197					187								
						183	239					224	197					187								
						184	238					225	197					187								
						183	237					223	197					187								
						240						222	198					187								
						239						219	198					187								
						240						217	198					187								
						239						215	198													
						241						204	198													
						236						201	199													
						235						201	198													
						234						200	199													
						236						201	201													
						233						201	201													
						234						197														
						232						196														
						236						198														
						232						200														
						235						201														
						231						199														
						234						199														
						232						200														
						231						201														
						228						201														
												202														
												201														
												202														
												204														